Development of Long Life Overlays for Existing Pavement Infrastructure Projects in New Jersey

> Northeast Asphalt User/Producer Group Meeting October 18, 2001

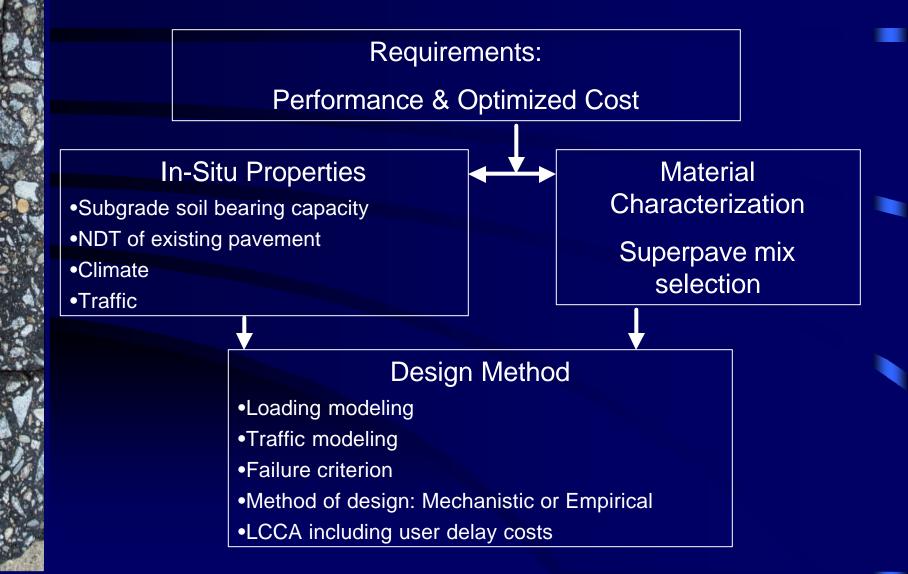
> > Robert Sauber Design Services <u>New Jersey</u> Department of Transportation

NJDOT Objectives "NJ First" Vision for 21st Century Transportation Systems

- Achieve the state of good repair for state's transportation system and maintain that system to ensure maximum useful life (fix it first)
- Eliminate the backlog of deficient pavement condition on state highways

Pavement Design Methodology

"Pavements are complex structures that are not fully understood"

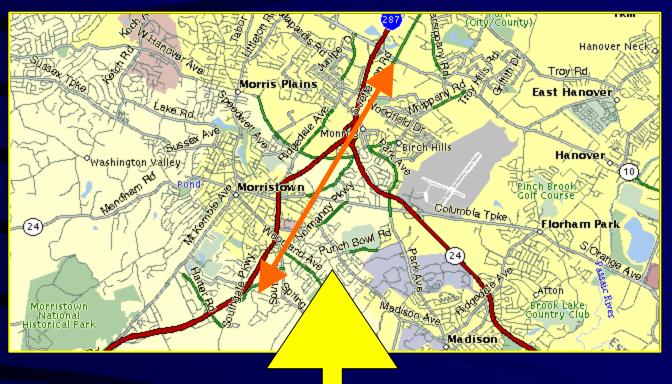


Introduction to I-287 Project

- North/South highway that provides a western bypass around NY City
- 3 major east/west highways intersect at this location: Rt. I-80, Rt.10 and Rt. 24
- Roadway geometry restricted due to location in the town of Morristown
- 24,000 trucks/day (2 way)
- Project limits: MP 35.5 to MP 38.8

Rt. I-287 Project Goals

- Construct HOV lanes to increase capacity and coincide with the opening of I-287 to the north
- Rehabilitate pavement structure with minimal impact on roadway profile
- Provide a durable wearing surface
- Construct while maintaining existing number of travel lanes during peak traffic hours



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New Brunswick

Rossmoor

Red Bank

Belma

White Plain

Elmont Long Beach

Fair Haven

Long Branch

Asbury Park

Paterson

ayreville Leonardo

Project Location

- Initial construction 1968
- Rehab design 1993

Rt. I-287 Pavement History

Pavement Composition

- 3" HMA Surface Course
- -7" HMA Base Course [stone mix]
- -8" Dense Graded Aggregate [crushed stone]
- 10" Subbase [graded sand]
- No rehabilitation up to this point

Rt. I-287 Design Data

- Design Data
 - -1993 ADT₂ = 110,190
 - -2013 ADT₂ = 170,830
 - -22% Total Trucks, 9% Heavy Trucks
 - 20 year ESALs = 50,000,000
 - Slow/standing loads due to periodic traffic congestion

Rt. I-287 Design Data

- Pavement age 26 years
- Subgrade soil: silty sand
- Frost penetration 36 inches
 Proposed Quantities
- 75,000 tons HMA polymer surface mix
- 225,000 tons HMA base mix

Rt. I-287 Pavement Condition

- 1994 Visual Condition Survey
 - Lanes 2 and 3
 - Moderate to high severity fatigue cracking
 - Wheel path longitudinal cracking
 - Some high severity patching
 - Rutting >1"
 - Lane 1
 - Low severity cracking
 - Rutting<1"

Typical Surface Appearance

Rt. I-287 Pavement Coring

- Initial indications were that cracks penetrated through all bound layers
- Coring results
 - Cracks originated at surface with majority stopping at the base layer (3" depth)
 - Materials testing
 - 25 Pavement cores

Penetration and Air Voids



REC. PEN	VOIDS	
16	5.5%	
40	4.9%	
22	6.8%	
25	9.3%	

Example of Surface Cracking



PHOTOGRAPH OF CORE

TOP

- CRACK

NEGATIVE ENCHANCED IMAGE

Pavement Distress

- Pavement is surface cracked
- Classical models do not help us to predict this distress
- Possibly a result of very hard binder in the surface mix

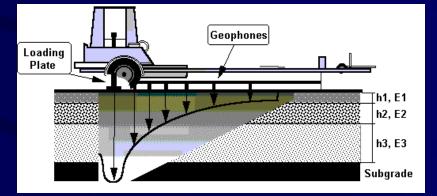
Pavement Models

- Classical Pavement Design
 - Fatigue Cracks Start at bottom
 - Pavement rutting controlled by sub-grade strain
- On Site
 - Extensively cracked pavement
 - Cracks originate at the top and restricted to top 3 inches
 - Few cracks through entire layer

Typically cracks assumed to start here!

Route I- 287 FWD Testing

- FWD testing was conducted on all traffic lanes to determine the stiffness of the pavement layers
- The stiffness of the combined asphalt layer (85 percentile deflection) were as follows:
 - NB1 7,100 MPa
 - NB2 5,600 MPa
 - NB3 4,600 MPa
 - SB1 7,600 MPa
 - SB2 5,300 MPa
 - SB3 4,900 MPa



- NB= North Bound, SB= South Bound, 1= fast lane, 3= slow lane.
- Lane 3 has considerably lower stiffness compared to lane 1.

FWD Structural Analysis

FWD testing

- Pavement structure generally good, slow lane $S_n = 5.7$
- Deflection testing after milling $S_n = 4.5$
- After resurfacing $S_n = 7.6$
- FWD and core analysis suggests that after removing distressed surface layers a structurally sound base remained

FWD Results

Lane 3 slow lane heavy traffic



= 4,750 MPa

Cracked top layer

Sound base of high stiffness Sound pavement structure with minimal cracking Lane 1 fast lane light traffic

Combined Stiffness

= 7,350 MPa

Rt. I-287 Pavement Rehabilitation

- Mill 3" depth (removes most cracks)
- Overlay
 - -2" HMA surface course, polymer modified
 - -2" minimum HMA base course [stone mix]
 - Test area with 1200 tons of NJ's first
 Superpave mix
 - Minimal modification needed to convert existing mixture to meet 12.5 mm Superpave requirements

Project Summary

- Adequate service life achieved with only a relatively thin overlay
- Existing structural capacity 7,000,000 ESALs
- Rehabilitated structural capacity 69,000,000 ESALs
- Superpave mix not much different than New Jersey's current "HD" mix
- 2001 PMS data indicates zero defects

Current Rt. I-287 Condition



Route I-78 History

- Route I-78 EB from MP 31 to MP 43 in New Jersey
- Rehabilitation project designed by NJDOT forces Jan 1998
- Original Construction 1970: 6"-7" HMA, 9"-13" crushed stone base, 12"-14" subbase
- Resurfaced in 1986 (mill 2", resurface 6")
- Initial pavement investigation visual survey & coring
- Core recovery: 1.5"-12" HMA
- Severely Distressed Pavement; high severity cracking and raveling

Route 78 EB

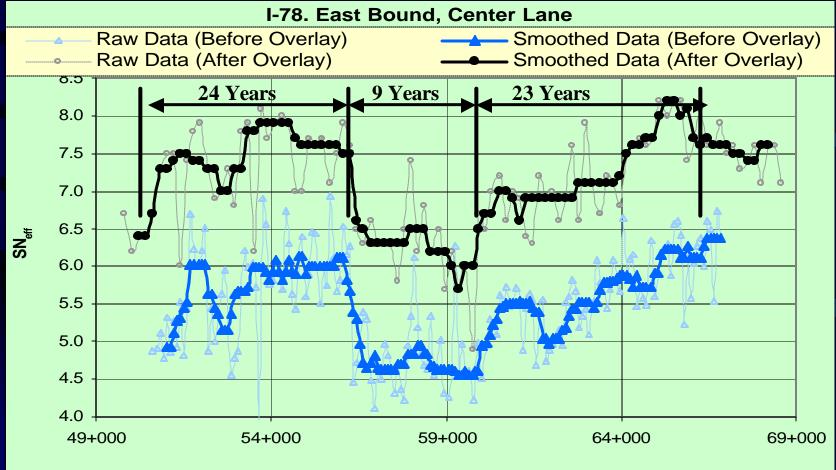
- The resurfacing project was designed based on material parameters estimated from a visual distress survey and pavement coring.
- Initial design 2" milling and 4" overlay (holding action)
- FWD added in construction plans
- FWD testing was performed to evaluate the effectiveness

Role of NDT on Rt. I-78 Project

Incorporation of FWD:

- Elastic modulus of HMA (E_{AC})
- Subgrade resilient modulus (M_R)
- Effective structural number (SN_{eff})
- SN_{eff} profile of project
- Overall pavement condition estimated service life
- Effectiveness of pavement treatment
 - structural increase from the overlay
- Detailed pavement analysis
 - in-situ material properties

FWD Typical Results Pavement Evaluation Route 78 EB MP 30.5 to MP 42.7



Station

Route I-78 FWD Evaluation

	Before Ov	erlay	After Overlay		
Lane					
	E _{ac} MPa (ksi)	SN _{eff}	E _{ac} MPa (ksi)	SN _{eff}	
Left	5799 (830)	5.6	8400 (1210)	7.1	
Center	3900 (570)	5.6	6100 (890)	7.1	
Right	6300 (900)	5.4	7900 (1150)	7.0	
Auxiliary	6600 (950)	5.5	6700 (970)	7.2	

Route I-78 Material Properties and Estimated Service Life

		Left Lane		Center Lane		Right Lane	
		Before Overlay	After Overlay	Before Overlay	After Overlay	Before Overlay	After Overlay
	20°C (ksi)	5300 (760)	7900 (1150)	3800 (550)	5900 (860)	5700 (800)	7600 (1100)
	le M _r kPa si)	11500 (11200)	69900 (10200)	88500 (12800)	75100 (10900)	72000 (10500)	69600 (10100)
MP30.7- 37.4	SN _{eff}	5.6	6.9	5.3	6.9	5.2	6.8
	Life in Years		13		13		12
MP37.4- 42.7	SN _{eff}	5.6	7.2	5.8	7.3	5.6	7.2
	Life in Years		21		23		21

The FWD

testing was performed both before and after milling and resurfacing of the HMA pavement. The FWD test data was back-calculated using the PADAL [] program to determine the elastic modulus of AC pavement (EAc), subgrade resilient modulus (IV&), and the effective structural number (SN,,) of the roadway. A follow-up design that was performed in accordance with AASHTO Guide for Design of Pavement Structures [2] indicated that the structural number of the pavement had increased an average of 1.6, with a service life of 15 to 19 years. FWD results also indicated that few sections of the roadway had higher deflections and needed more extensive rehabilitation. The service life of the overlay for these sections was estimated to be approximately 12 to 13 years. highlight the importance of FWD testing and the back-calculation procedure as a tool for optimizing project level design efforts. This project confirmed that FWD testing is instrumental in identifying deficient sections, optimizing pavement treatments, and therefore providing the most costeffective solution for those charged with managing their project resources. Demonstrating the success of using FWD, NJDOT incorporated this approach for the 12-mile segment of Route 78 in the WB direction the following year.